

High Current Density and Low Thermal Conductivity of Atomically Thin Semimetallic WTe_2

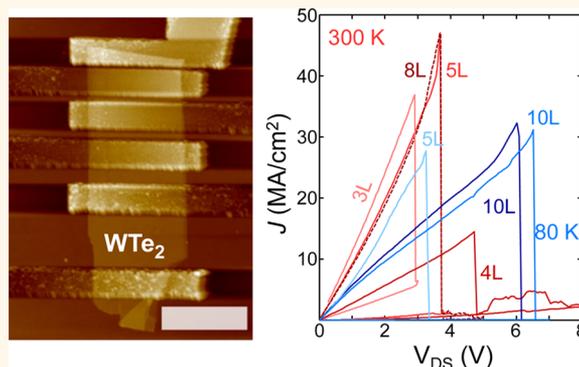
Michal J. Mleczko,[†] Runjie Lily Xu,[†] Kye Okabe,[†] Hsueh-Hui Kuo,[‡] Ian R. Fisher,[§] H.-S. Philip Wong,[†] Yoshio Nishi,[†] and Eric Pop^{*,†,||}

[†]Department of Electrical Engineering, [‡]Department of Materials Science and Engineering, [§]Department of Applied Physics, and ^{||}Precourt Institute for Energy, Stanford University, Stanford, California 94305, United States

S Supporting Information

ABSTRACT: Two-dimensional (2D) semimetals beyond graphene have been relatively unexplored in the atomically thin limit. Here, we introduce a facile growth mechanism for semimetallic WTe_2 crystals and then fabricate few-layer test structures while carefully avoiding degradation from exposure to air. Low-field electrical measurements of 80 nm to 2 μm long devices allow us to separate intrinsic and contact resistance, revealing metallic response in the thinnest encapsulated and stable WTe_2 devices studied to date (3–20 layers thick). High-field electrical measurements and electrothermal modeling demonstrate that ultrathin WTe_2 can carry remarkably high current density (approaching 50 MA/cm^2 , higher than most common interconnect metals) despite a very low thermal conductivity (of the order $\sim 3 \text{ W m}^{-1} \text{ K}^{-1}$). These results suggest several pathways for air-stable technological viability of this layered semimetal.

KEYWORDS: two-dimensional atomic layers, semimetals, transition metal dichalcogenides, current density, thermal conductivity, environmental stability



The preceding decade saw much interest in two-dimensional (2D) nanomaterials, often exhibiting distinct evolution of chemical and physical properties as material thickness is scaled from layered bulk to individual atomic or molecular monolayers.^{1–3} While semiconducting 2D materials have received much attention, layered 2D semimetals other than graphene have been relatively underexplored in the atomically thin limit. Materials such as $\beta\text{-MoTe}_2$ and WTe_2 stabilize as semimetals in a distortion of the octahedral 1T (CdI_2 structure) geometry, with in-plane buckled chains formed by pairs of Mo/W atoms dimerizing in intermetallic charge–exchange,^{4–6} while van der Waals bonding dominates the interlayer interaction. Whereas MoTe_2 may be synthesized in both 2H and 1T polytypes, or reversibly switched between the two as a function of temperature or strain,^{7,8} WTe_2 has been known since the 1960s to adopt an orthorhombic structure with the $Pmn2_1$ space group (sometimes called “Td”), irrespective of growth conditions^{4–6,9,10} or conventional strain,⁸ as the heaviest of the group VI dichalcogenides.

Despite the inaccessibility of a semiconducting phase, semimetallic WTe_2 has received renewed attention from the experimental observation of nonsaturating magnetoresistance in

bulk samples, in excess of 13 million percent up to 60 T at 0.53 K.¹¹ This behavior was attributed to perfect compensation between balanced electron and hole populations at the Fermi surface below 150 K, projected to persist down to individual monolayers.^{12,13} Recent studies have also identified WTe_2 as a potential contact for 2D semiconductors, with a relatively low work function ($\Phi < 4.4 \text{ eV}$) among 2D metals,¹⁴ recently applied in realizing unipolar n-type transport in the typically ambipolar semiconductor WSe_2 .¹⁵ Layer-dependent experiments of any kind are nonetheless limited,^{16–19} due to a lack of geological sources, challenges in precursor purification during bulk crystal growth,^{10,11} as well as observed degradation (oxidation) of thin layered tellurides with exposure to ambient oxygen and moisture.^{16,19,20} In particular, Wang and colleagues studied magnetotransport in uncapped flakes down to bilayer thickness,¹⁹ reporting an insulating regime in sub-six-layer samples attributed to oxidation-induced disorder from ambient exposure.

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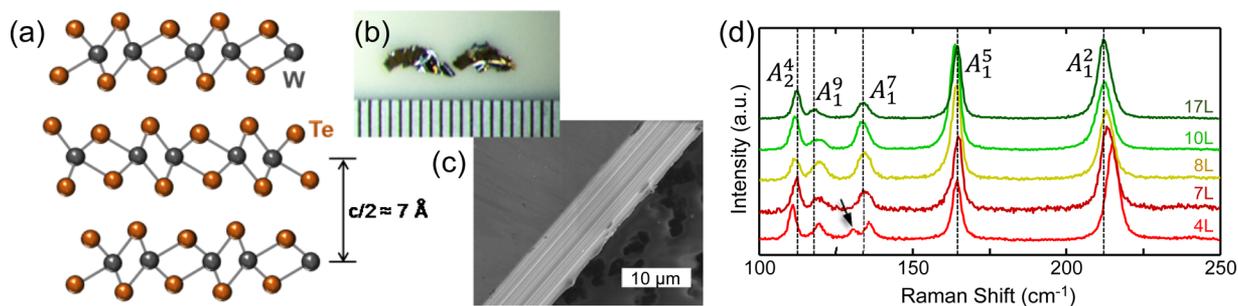


Figure 1. (a) Schematic cross section of the semimetallic orthorhombic phase of WTe_2 .^{5,11,18} (b) Bulk WTe_2 crystals grown by CVT, with millimeter increments for scale. (c) SEM micrograph of grown bulk crystal displaying layered structure at the edge. (d) Raman spectra of ALD-capped few-layer WTe_2 , labeling typically observed modes (Horiba Labram, 532 nm laser at 2.5 mW power). The arrow marks the A_1^8 mode, which appears in our thin four-layer sample.

In this work, we first synthesize bulk WTe_2 crystals by a facile growth method employing commercially available molecular powders, and then we isolate few-layer flakes in an inert environment (Methods and Figure S1). Test devices are fabricated in a manner avoiding any open-air exposure of channel regions, ultimately encapsulating devices *in situ* with AlO_x by atomic layer deposition (ALD), as described in the Methods section. This stabilizes ultrathin WTe_2 against ambient degradation, evidenced by spectral analysis of vibrational modes and chemical bonding, preserving Ohmic conduction at high current densities. Electrical characterization is performed on (capped and stable) 3- to 20-layer WTe_2 devices using the transfer length method (TLM) approach, separating the contributions of intrinsic and extrinsic (contact) resistance from 80 to 300 K. High-field measurements (up to breakdown) reveal large current densities approaching $50 \text{ MA}/\text{cm}^2$, in the range of relevance for technological applications.^{21–23} By comparison with a self-heating model, we are also able to estimate the in-plane thermal conductivity of WTe_2 . This study represents the successful stabilization and electro-thermal characterization of intrinsic WTe_2 approaching the ultimate thickness limit, and could facilitate exploration of further fundamental properties, as well as potential device contacts, spintronic, memory, and interconnect applications.

RESULTS AND DISCUSSION

Fabrication and Characterization. Bulk crystals of WTe_2 (Figure 1a) were grown directly by chemical vapor transport (CVT) of a commercial molecular powder (American Elements WTe_2 , 99.5%), with no need for chemical or thermal precursor pretreatment, using elemental iodine as a transport agent (see the Methods section). We achieved a high yield of few-millimeter-sized crystals, exhibiting both ribbon- and platelet-like morphologies with clear evidence of layered structure under mechanical cleavage or scanning electron microscope (SEM) inspection (Figure 1b,c). Electron microprobe analysis (EMPA) confirmed a stoichiometry of $\text{WTe}_{2.05}$ with negligible levels of metal contaminants throughout bulk samples. We then mechanically exfoliated few-layer WTe_2 flakes onto 90 nm SiO_2 on p^{++} Si substrates under an inert atmosphere (a nitrogen-purged glovebox; O_2 and H_2O below 3 ppm at their highest levels) and initially capped them with a 300 nm film of poly(methyl methacrylate) (PMMA), serving both as protective coating and resist for electron-beam (e-beam) lithography.

Contacts were lithographically defined, developed, and metalized with 20 nm Ti/20 nm Au, such that exposed device contact surfaces saw cleanroom air for less than 5 min before

transfer into a load-locked e-beam evaporator (base chamber pressure $\sim 10^{-8}$ Torr). To mitigate the possibility of channel oxidation, we performed resist and metal lift-off in another nitrogen glovebox connected to a thermal ALD chamber where, after lift-off, we immediately deposited ~ 15 nm of amorphous AlO_x *in situ* by alternating trimethylaluminum (TMA) and H_2O pulses at 150°C . Inspection by optical and atomic force microscopy (AFM) revealed uniform nucleation of this capping dielectric (Figure 2a,b), with identical root-mean-square roughness on flakes and the surrounding oxide (<0.4 nm). The smoothness of the capping film facilitated layer counting in flakes directly from AFM height profiles, uniformly measured as integer multiples of the interlayer spacing of ~ 0.704 nm^{4,5} with an additional ~ 0.2 nm offset.

ALD-capped WTe_2 nanosheets were found to produce a characteristic, layer-dependent Raman response under illumination from a low-power 532 nm wavelength laser (Figure 1d), consistent with previous reports,^{16–19} and lacking any features associated with metal-oxide formation on tungsten dichalcogenides.^{24,25} The orthorhombic structure of WTe_2 results in a richer set of Raman-active vibrational modes than the simple A_{1g} and E_{2g} (cross- and in-plane) pairing in 2H-layered crystals; a total of five modes are identified in the range of 100 – 250 cm^{-1} , with bulk values delineated according to the convention of ref 17, corresponding primarily to vibrations of Te atoms around an expanded unit cell of a W–W dimer. These soften and stiffen to varying degrees as the layer number is reduced below 10, closely matching known theoretical and experimental values.^{17–19} An additional mode appears only in our thin four-layer sample, as a blue shift of the bulk A_1^7 mode¹⁸ exposes a 130.5 cm^{-1} shoulder peak (marked by an arrow in Figure 1d). This new feature represents the A_1^8 mode identified exclusively in this range by ref 17.

We utilized the encapsulation to prevent ambient oxidation of ultrathin WTe_2 , and ALD alumina was chosen for its compatibility with standard microfabrication and effectiveness as an oxygen and moisture barrier (also recently applied for environmental stability of few-layer black phosphorus^{26,27}). Grown on devices whose channels had only seen an inert nitrogen atmosphere (Figure 2a,b), 15 nm AlO_x films were found to significantly improve device yield and preserve Ohmic response with no noticeable current degradation after 1 week (Figure 2c). In comparison, uncapped devices measured immediately after in-air metal lift-off manifested current nonlinearity at moderate source–drain biases and significant decline in performance over several days—even when stored in partially deoxygenated environments (e.g., a tabletop drybox).

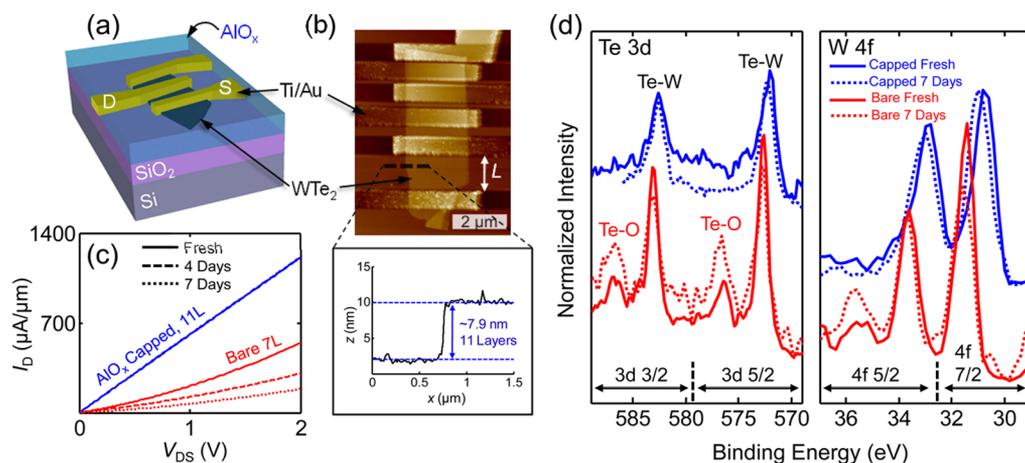


Figure 2. (a) Schematic of AlO_x -capped WTe_2 TLM structures on 90 nm SiO_2 (on Si) with Ti/Au contacts. (b) AFM micrograph of fabricated WTe_2 TLM structures showing five device channel lengths (from 85 to 1500 nm) and six electrodes, capped with ~ 15 nm AlO_x by ALD. AFM height profile (bottom inset) was extracted along the dotted line. (c) Time-dependent degradation of current vs voltage (I_D – V_{DS}) in AlO_x -capped (11 layer, $L = 0.5 \mu\text{m}$) and uncapped (7 layer, $L = 0.46 \mu\text{m}$) devices. The ALD-capped devices are air-stable for over 1 week, whereas the bare (uncapped) devices degrade within hours or days. (d) High-resolution XPS of ALD-capped and bare multilayer WTe_2 flakes on SiO_2/Si substrates; ambient degradation is visible in the formation of Te–O subpeaks and a binding energy shift of W 4f peaks, suggesting partial WO_3 bonding character.

Such degradation is consistent with increased charge trap density from the progressive oxidation of the top-most WTe_2 layers, which we evaluated by high-resolution X-ray photoelectron spectroscopy (XPS) in Figure 2d.

Oxidation of uncapped crystals is evident in the Te 3d spectra of both freshly cleaved and aged multilayers on SiO_2/Si , most prominently in the appearance of secondary peaks across the $3d_{3/2}$ and $3d_{5/2}$ energy range, matching reference values for Te(IV)–O binding in TeO_2 .^{28,29} These features increase in intensity with time relative to Te–W bonds, matching a trend recently observed in ref 16, though they are entirely absent on surfaces probed through the AlO_x capping. There, only W bonding is measured even after 7 days of storage. Ancillary evidence is provided in the upward energetic shift of W 4f peaks in uncapped samples, by an average ~ 0.8 eV relative to capped flakes, and the appearance of a high-energy shoulder, suggesting a partial WO_3 bonding character induced through atmospheric exposure. Layered WO_3 is the oxide most readily formed on W dichalcogenide crystals,^{24,25} producing XPS W 4f reference peaks measured an average of 2–3 eV higher^{30,31} in binding energy than those of comparatively closely spaced WS_2 and WSe_2 ^{31–33} used here as analogues for WTe_2 . Our findings indicate significant chemical degradation of uncapped layers during the ~ 1 h period of ambient exposure between glovebox-based exfoliation and XPS measurement, despite prior studies observing constant optical contrast for exposed few-layer samples on the order of 1 day.¹⁹ This supports the conjecture of oxidation-induced disorder driving a metal-to-insulator transition in resistivity when the WTe_2 thickness is reduced below six layers,¹⁹ a regime avoided through careful encapsulation in all our thinner samples discussed below.

Low-Field Electrical Transport. We performed electrical characterization *via* two-terminal and TLM test structures, with channel lengths L from 80 nm to 2 μm , as shown in Figure 2a,b. As expected for carrier-rich semimetallic devices, the Si back-gate had a negligible ($<5\%$) effect on current modulation (Figure S2a), and the remainder of electrical measurements was carried out at zero gate bias. Figure 3a shows the linear fits for a TLM test structure, over the 80–300 K temperature range.

Plotting the measured resistance normalized by width, $RW = R_S L + 2R_C$, yields a slope R_S as the intrinsic sheet resistance and the intercept $2R_C$ as the total contact resistance (L and W are the length and width of the WTe_2 channel). Figure 3b presents a summary of TLM-extracted resistivity ρ in the range of 0.4–1.4 $\text{m}\Omega\cdot\text{cm}$ (at room temperature) for WTe_2 devices of different layer thicknesses. Most ultrathin devices display metallic behavior (ρ increasing with T), consistent with prior reports of bulk resistivity for synthetic WTe_2 .^{1,18,34} Only the 17-layer device exhibited monotonic decline in ρ with increasing T ; however, this was one of the most resistive TLM structures probed, thus its temperature-dependent behavior could be more indicative of defect-limited hopping rather than phonon-limited transport (as for the devices with lower ρ).

Interestingly, no clear layer dependence of resistivity emerges for the thickness range probed here; this could be due to different crystalline orientations of the devices, as buckled W chains break the 2D symmetry of the layer plane with a preferred directionality.^{4–6} This has been noted in scanning tunneling microscopy (STM) measurements of aligned zigzag features on cleaved WTe_2 surfaces³⁵ and a strong variation on magnetotransport in bulk ribbons with the angle of the applied field.¹¹ Thickness invariance in this range is also consistent with recent measurements of an effectively three-dimensional electronic structure in WTe_2 ,^{36,37} with only moderate Fermi surface anisotropy in 2D layers attributed to increased interlayer coupling from the described lattice distortion. Room-temperature resistivity remains an order of magnitude greater than that of layered band metals in bulk,^{1,9} including most group V (V, Nb, Ta) disulfides, selenides, and tellurides. It nonetheless remains comparable to that of bulk WTe_2 ,^{18,34} unlike the 10-fold or greater increase of ρ in metals like 1T-TaS₂ in the few-nanometer thickness regime.^{38,39}

Extracted contact resistances for 20 nm Ti/20 nm Au leads (Figure 3c) also show no clear dependence on layer number, with mean R_C spanning a range of 500–600 $\Omega\cdot\mu\text{m}$ over the 80–300 K temperature range. (Figure S2c displays the temperature dependence of R_C , which increases with temperature like the resistivity.) The contact resistance to ultrathin

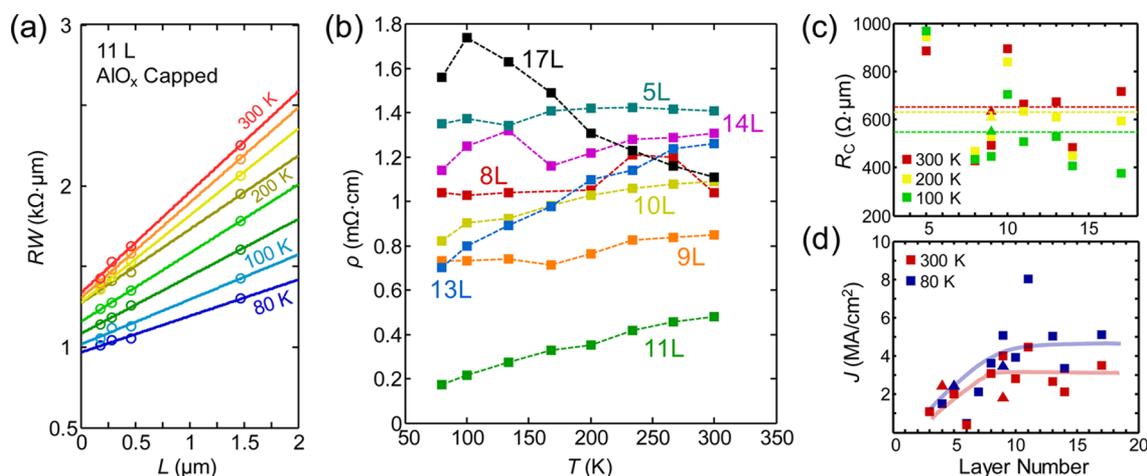


Figure 3. (a) Typical TLM plot of AlO_x -capped, 11-layer WTe_2 devices presenting the total resistance (normalized by width) vs channel length L ; lines are a numerical fit to measured values (symbols). **Figure 2a,b** displays the typical TLM geometry. The vertical intercept yields $2R_C$, and the slope yields R_S . (b) Measured temperature dependence of resistivity for AlO_x -capped WTe_2 devices with 5–17 layers, derived from TLM sheet resistance. (c) Contact resistance between WTe_2 and 20 nm Ti/20 nm Au contacts for different temperatures and layer numbers, extracted from TLM measurements. Dashed lines denote average R_C values at 100, 200, and 300 K. (d) Low-field ($F = 4000 \text{ V cm}^{-1}$) current density in capped WTe_2 devices at 80 and 300 K, corrected for contact resistance. Lines are guides for the eye; different symbols represent different samples.

WTe_2 found here is near the lower end of reported resistances for evaporated metals on transition metal dichalcogenides ($0.5\text{--}2 \text{ k}\Omega\text{-}\mu\text{m}$) without chemical doping or lattice-level modification.^{40,41}

Figure 3d presents the current density J at 80 and 300 K for all measured thicknesses,⁴² at low intrinsic field (4000 V/cm ; equivalent to 1 V across a $2.5 \mu\text{m}$ channel length). Despite the aforementioned variability obscuring an explicit layer dependence, the current density J appears to increase up to 9–11-layer device thickness, beyond which J saturates. A gradual fall-off in current density might be expected for thicker, metallic layered crystals with top contacts (*i.e.*, tens of layers to bulk) due to interlayer resistance limiting current flow to the top-most layers. In contrast, the cross-plane current distribution in few-layer graphene or semiconducting 2D materials is determined by competing effects from electrostatic gating, top-down charge injection, and interlayer electrostatic screening.^{43,44} For a carrier-rich (semi-) metallic 2D crystal, dielectric screening limits the charge injected into lower layers from top contacts as the thickness is increased, effectively confining current to the top-most layers in the absence of direct edge injection. Underlying strata serve primarily to screen-out any substrate (*e.g.*, oxide) charge fluctuations in approaching bulk transport limits.⁴³ Absence of this screening in the thinnest, most sensitive samples (≤ 5 layers) explains the lower measured current densities and slightly higher TLM-extracted contact resistance.

High-Field Transport. We next examine high-field, coupled electrical and thermal transport in our WTe_2 devices, as summarized in **Figure 4**. First, we note that for modeling purposes of a given device, $\rho(T)$ can be fit as a function of temperature by a cubic polynomial (**Figure S2b**). This facilitates current calculation as a function of temperature, $I(T) = V/R(T)$, self-consistently with a self-heating (SH) model. To estimate the average temperature increase, we can express the thermal resistance per unit length from the WTe_2 channel to the substrate as⁴⁵

$$g^{-1} = \frac{R_{\text{Cox}}}{W} + \left\{ \frac{\pi k_{\text{ox}}}{\ln[6(t_{\text{ox}}/W + 1)]} + \frac{k_{\text{Si}}}{t_{\text{ox}}} W \right\}^{-1} + \frac{1}{2k_{\text{Si}}} \left(\frac{L}{W_{\text{eff}}} \right)^{1/2} \quad (1)$$

where t_{ox} is the SiO_2 thickness, k_{ox} and k_{Si} are the thermal conductivities of SiO_2 and Si (including their temperature dependence;⁴⁶ see **Supporting Information** section 3), and W_{eff} is an effective width of the heat dissipation path through the Si substrate.⁴⁵ The equation above represents the series combination of three terms: the thermal resistance of the $\text{WTe}_2\text{--SiO}_2$ interface R_{Cox} , the spreading thermal resistance into the SiO_2 ,⁴⁷ and the spreading thermal resistance into the Si substrate (**Figure 4a** inset).

The average temperature increase due to Joule heating is $T = T_0 + I(T)V\mathcal{R}_{\text{th}}$, where T_0 is the ambient temperature and $\mathcal{R}_{\text{th}} \approx 1/(gL)$ is the total thermal resistance for “long” devices,⁴⁸ much longer than the thermal healing length L_{H} along our WTe_2 devices. Here, $L_{\text{H}} = (kWt/g)^{1/2} \approx 70\text{--}150 \text{ nm}$ (as we will see in the following discussion), where t is the thickness and k is the lateral thermal conductivity of WTe_2 . **Figure 4c** shows that this model with SH can correctly reproduce the decrease in current at high field, whereas the model without SH cannot capture this behavior for a “long” device with $L \approx 750 \text{ nm}$. The $\text{WTe}_2\text{--SiO}_2$ thermal interface resistance was used as a fitting parameter here, yielding an estimated $R_{\text{Cox}} \approx 3 \times 10^{-8} \text{ m}^2 \text{ KW}^{-1}$, which is similar to the values of R_{Cox} for graphene– SiO_2 interfaces.⁴⁹

We can also extend this simple SH model to include heat loss from WTe_2 to the AlO_x capping layer and to the Ti/Au contacts. This is primarily applicable to our “shorter” devices (compared to L_{H}), where more heat flows laterally into the metal contacts. We can express the peak (maximum) temperature along the WTe_2 device as a function of the input power P and other thermal parameters as

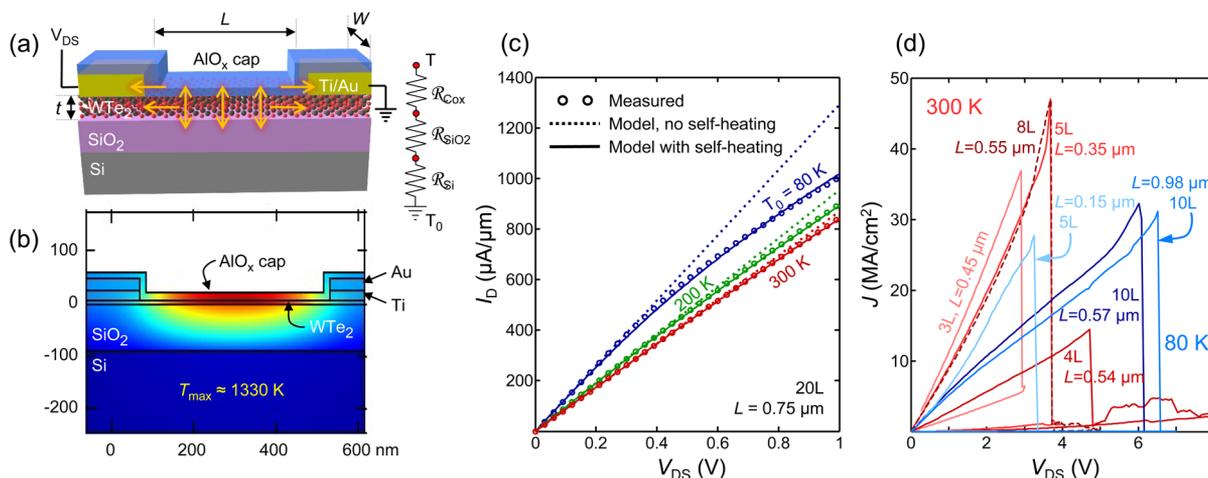


Figure 4. (a) WTe₂ device schematic, with arrows showing pathways for heat sinking during high-field operation. Inset shows simplified thermal resistance model for vertical heat flow, which dominates in longer devices ($L \gg L_H$). (b) Thermal simulations (COMSOL) were used to validate the analytic thermal model (Supporting Information section 5). Here, the simulation is shown just before WTe₂ breakdown. (c) Measured (symbols) and simulated (lines) current vs voltage for an uncapped 20-layer WTe₂ device. Solid lines modeled with self-heating (SH) model, dashed lines are without SH. (d) Measured current density vs voltage up to thermal breakdown of ALD-capped WTe₂ devices at 80 K (blue) and 300 K (red) ambient conditions in a vacuum probe station ($\sim 10^{-5}$ Torr). The maximum current density approaches 50 MA/cm², almost an order of magnitude higher than typical bulk metal interconnects (e.g., Al, Cu). SEM images after device breakdown are shown in Figure S6.

$$T_{\max} = T_0 + P \left(\frac{1}{gL} \right) \left(\frac{1 + gL_H \mathcal{R}_T x - 1/\cosh[L/(2L_H)]}{1 + gL_H \mathcal{R}_T x} \right) \quad (2)$$

where $x = \tanh[L/(2L_H)]$. Similarly, we can also express the average temperature (T_{avg}) along the WTe₂:

$$T_{\text{avg}} = T_0 + P \left(\frac{1}{gL} \right) \left(\frac{1 + gL_H \mathcal{R}_T x - 2xL_H/L}{1 + gL_H \mathcal{R}_T x} \right) \quad (3)$$

where $\mathcal{R}_T = L_{\text{HM}}/[k_m t_m (W + 2L_{\text{HM}})]$ is the thermal resistance of the metal contacts, $L_{\text{HM}} = (t_m t_{\text{ox}} k_m / k_{\text{ox}})^{1/2}$ represents the thermal healing length into metal contacts of thickness t_m and thermal conductivity k_m , and $T_0 = 80$ or 300 K. Equations 2 and 3 reduce to that of the “long” device [$T_{\max} \approx T_{\text{avg}} \approx T_0 + P/(gL)$] when $L \gg L_T$, and the temperature profile is flat from source to drain.⁵⁰ The expressions can also be simplified when contacts are assumed to be perfect heat sinks ($\mathcal{R}_T = 0$), which is often a reasonable approximation.⁵⁰ The analytic model given by eqs 1–3 is applicable to most metallic interconnects, not just to WTe₂, and it is validated here with finite-element (COMSOL) simulations of the device structure in Figure 4b. (More simulation results are shown in Supporting Information section 5.)

Figure 4d displays several measured I – V curves up to breakdown of our WTe₂ devices, with high lateral V_{DS} (the higher resistivity at 80 K is due to intersample variability of particular 5- and 10-layer flakes). We find that ALD-capped WTe₂ devices can reach up to 30–50 MA/cm² current densities, in excess of the 10–20 MA/cm² benchmark for VLSI interconnect stress testing.^{21–23} We also obtain current densities of >30 MA/cm² in two WTe₂ nanoribbons (~ 50 nm wide) shown in Figure S7. These current densities are larger than typical values for Al and Cu, which are several MA/cm², and are similar to bulk W films at several tens of MA/cm².^{51–53} Among atomically thin semimetallic layers, only graphene can withstand higher current densities, typically hundreds of MA/cm² and approaching 1 GA/cm² for aggressively scaled

nanoribbons.⁴⁵ SEM imaging of most failed devices (Figure S6) showed breakdown near the device midpoints, with intact metal contacts, suggesting WTe₂ failure at the point of maximum temperature and good contact resistance up to high bias.

Our thinnest ALD-capped devices (3–5 layers) in Figure 4d show Ohmic response and breakdown current densities (up to ~ 50 MA/cm²) comparable to thicker ones. Taken together with Figure 3c,d, these findings are in contrast with a prior study on uncapped samples,¹⁹ which reported a sharp increase of resistivity and insulating behavior in ultrathin WTe₂ (<6 layers). As another reference point, layered metallic TaSe₂ supports lower peak current densities of 19 ± 8 MA/cm² in conventionally fabricated (also uncapped) devices of ~ 12 nm thickness, with unreliable measurements in much thinner flakes.⁵⁴ Our experiments thus reinforce the importance of encapsulation with ALD and avoiding exposure to oxygen and moisture during processing (see Methods). In addition, our simulations (Figures S4 and S5) also suggest that the encapsulation layer partly aids lateral heat spreading to the contacts during high-field transport, assisting the higher current densities. Encapsulating WTe₂ devices with a higher thermal conductivity material (hexagonal boron nitride, h-BN, instead of ALD) or placing them on a better heat-sinking substrate (e.g., 30 nm SiO₂) could further increase the current densities by another 10–25% (Table S2).

Thermal Conductivity Estimate. We can also utilize these self-heating studies at high field to estimate the lateral thermal conductivity k of WTe₂, following the work of Liao *et al.*,⁴⁷ with our updated model from eqs 1–3 above. The input power is $P = I_D(V_{\text{DS}} - 2I_D R_C)$, where R_C is the electrical contact resistance and $T_{\max} \approx 1300$ K is the WTe₂ breakdown temperature (the melting temperature of WTe₂).⁵⁵ For devices capped by ALD, we must be careful to account for partial lateral heat sinking through this capping layer. Thus, we modify the lateral healing length to $L_H = (k_{\text{eff}} W t / g)^{1/2}$, where the effective thermal conductivity, k_{eff} , is the parallel combination of lateral heat flow along the WTe₂ and the ALD capping ($t_{\text{cap}} \approx 15$ nm and $k_{\text{cap}} \approx$

$4 \text{ Wm}^{-1} \text{ K}^{-1}$ at high temperature near T_{max} .^{56,57} Once k_{eff} is estimated from our SH model, the thermal conductivity of WTe_2 can be deduced from $k = k_{\text{eff}} - k_{\text{cap}}(t_{\text{cap}}/t)$.

We note that in this high-temperature breakdown model we cannot fit the thermal conductivity k and \mathcal{R}_{Cox} independently; nonetheless, values consistent with all our measured device breakdowns are fit at $k = 2.5\text{--}3.5 \text{ Wm}^{-1} \text{ K}^{-1}$ for $\mathcal{R}_{\text{Cox}} = 5 \times 10^{-9} \text{ m}^2 \text{ KW}^{-1}$ and up to $k = 9\text{--}11 \text{ Wm}^{-1} \text{ K}^{-1}$ for $\mathcal{R}_{\text{Cox}} = 10^{-8} \text{ m}^2 \text{ KW}^{-1}$ (see discussion in Supporting Information section 3). \mathcal{R}_{Cox} values are expected to be smaller at high temperatures (near $T_{\text{max}} \approx 1300 \text{ K}$) than the earlier $3 \times 10^{-8} \text{ m}^2 \text{ KW}^{-1}$ estimate at $80\text{--}150 \text{ K}$, due to higher phonon occupation.

The lateral thermal conductivity estimated here is greater than that measured by Jana *et al.* on bulk polycrystalline samples of WTe_2 ($\sim 1 \text{ Wm}^{-1} \text{ K}^{-1}$),¹⁸ suggesting higher material quality in exfoliated monocrystalline flakes, within the range computed by Liu *et al.*⁵⁸ The electronic contribution is 10–30% of the overall thermal conductivity, based on estimates with the Wiedemann–Franz law (Figure S3). The lower bound of our estimated k is less than one-half the maximum lattice conductivity of $\sim 9 \text{ Wm}^{-1} \text{ K}^{-1}$ along the [100] (in-plane) WTe_2 direction from first-principles calculations.⁵⁸ Its magnitude and variation between devices are nonetheless consistent with the anisotropy expected between multiple in-plane (*i.e.*, relative to $W\text{--}W$ dimer chain orientation) and cross-plane k values, suggesting a strong role of structural asymmetry on thermal transport in such crystals. Orientation mapping of devices and ancillary measurement techniques (*e.g.*, time-dependent thermoreflectance across flakes of varying thickness) are needed to elucidate the directional dependence of this parameter.⁵⁹

CONCLUSION

In conclusion, we studied electrical and thermal transport in ultrathin (3–20 layers) semimetallic WTe_2 devices. The WTe_2 crystals were grown from a commercial molecular powder and exfoliated as few-layer flakes in an inert atmosphere, on which we fabricated TLM test structures. Glovebox-based processing and *in situ* encapsulation with an ALD alumina layer protected devices from ambient oxidation, with this process being essential for obtaining good transport and stability across several weeks for the thinnest (3–6 layers) devices. The intrinsic resistivity of our ultrathin WTe_2 is $10^{-4}\text{--}10^{-3} \Omega\text{-cm}$ between 80 and 300 K, with mean contact resistances of 400–600 $\Omega\text{-}\mu\text{m}$. The maximum current density ranged from 30 to 50 MA/cm^2 in encapsulated, air-stable devices (including WTe_2 nanoribbons), which is higher than that achievable in most bulk metal interconnects. Comparison of high-field breakdown with an analytical self-heating model estimated low intrinsic thermal conductivity around $3 \text{ Wm}^{-1} \text{ K}^{-1}$ for such ultrathin WTe_2 devices. Additional finite-element simulations indicate that the maximum current density of these interconnects could be increased by capping with a higher thermal conductivity material (such as h-BN) or placing them on better heat-sinking substrates (*e.g.*, thinner SiO_2).

It is tempting to assign thermoelectric applications to a good conductor of electricity with poor thermal properties; however, the thermopower (Seebeck coefficient) of WTe_2 is relatively small due to its semimetallic nature.^{18,34} Nevertheless, applications in phase-change memory particularly demand nanoscale electrodes with good current density and poor thermal conductivity^{60,61} to lower the programming energy per

bit. In addition, nanostructured WTe_2 could also be a promising candidate for other applications, including as 2D contacts to layered transistors,^{14,15,60} in magnetic memory,^{11,19} sensors, and spintronics.^{62,63}

METHODS

Material Growth and Fabrication. Bulk WTe_2 crystals were grown by CVT of a WTe_2 molecular powder (American Elements, 99.5%) sealed in a quartz tube evacuated under argon, with elemental iodine (Alfa Aesar, 99.99+%) added at 5 mg/cm^3 . Growth took place for 14 days along an 11 cm transport length, in a single-zone furnace with a central temperature of $900 \text{ }^\circ\text{C}$ and a $\sim 100 \text{ }^\circ\text{C}$ thermal gradient (Figure S1). Few-layer flakes were exfoliated onto 90 nm SiO_2 on p^{++} Si substrates within the inert atmosphere of a nitrogen glovebox, using low-residue thermal release tape, and were solvent-cleaned and capped *in situ* by spin-coating a layer of PMMA (Microchem A5 950k). Certain substrates were subject to a weak O_2 plasma exposure (2 min at 60 W, 250 mTorr) to promote adhesion of thinner flakes. The protective PMMA layer also served as a resist for electron-beam lithography of top contacts (Raith 150, 20 kV), developed and transferred within <5 min into load-locked metal evaporators (Kurt J. Lesker or AJA, both electron beam) for deposition of 20 nm Ti/20 nm Au. Lift-off was performed with acetone/2-propanol in a nitrogen glovebox directly connected to a Cambridge Savannah Thermal ALD system. Thus, ALD encapsulation (with $\sim 150 \text{ \AA}$ of alumina deposited by alternating TMA and water cycles at $150 \text{ }^\circ\text{C}$, first saturating surfaces with 10 leading TMA cycles) was accomplished without exposing the devices to ambient air.

Characterization. Compositional analysis on bulk crystals was performed with a JEOL JXA-8230 electron probe microanalyzer. Individual flakes were profiled with an AFM (Veeco Dimension 3100) and Raman spectroscopy (Horiba Labram, 532 nm laser source). High-resolution XPS analysis was performed in a Phi 5000 VersaProbe, calibrated to surface C 1s peaks, with capping layers etched away by *in situ* Ar^+ sputtering with iterative signal collection, such that an Al signal was monitored to prevent damage to the flake–alumina interface. Bulk crystals and devices were imaged at high resolution with a FEI XL30 Sirion and the SEM mode of a Raith 150. Electrical characterization was performed in a Janis cryogenic probe station (chamber pressure = 10^{-6} to 5×10^{-5} Torr) cooled with closed-loop liquid nitrogen and connected to a Keithley 4200-SCS parameter analyzer.

ASSOCIATED CONTENT

Supporting Information

The Supporting Information is available free of charge on the ACS Publications website at DOI: 10.1021/acsnano.6b02368.

Figures showing the temperature dependence of two-terminal resistivity and its gate dependence; elucidation of the self-heating model and thermal conductivity estimates; temperature evolution of extracted contact resistance and the electronic contribution to thermal conductivity; finite-element (COMSOL) simulations of device temperatures for various substrate oxide thicknesses and encapsulation layer configurations; SEM analysis of bulk flakes and laterally scaled nanoribbons following breakdown; discussion of WTe_2 breakdown mechanisms (PDF)

AUTHOR INFORMATION

Corresponding Author

*E-mail: epop@stanford.edu.

Notes

The authors declare no competing financial interest.

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Supplementary Information

High Current Density and Low Thermal Conductivity of Atomically Thin Semimetallic WTe₂

Michal J. Mleczko¹, Runjie (Lily) Xu¹, Kye Okabe¹, Hsueh-Hui Kuo², Ian R. Fisher³, H.-S. Philip Wong¹,
Yoshio Nishi¹, Eric Pop^{1,4,*}

1. Department of Electrical Engineering, Stanford University, Stanford CA 94305, USA

2. Department of Materials Science and Engineering, Stanford University, Stanford CA 94305, USA

3. Department of Applied Physics, Stanford University, Stanford CA 94305, USA

4. Precourt Institute for Energy, Stanford University, Stanford CA 94305, USA

1. Growth and Exfoliation

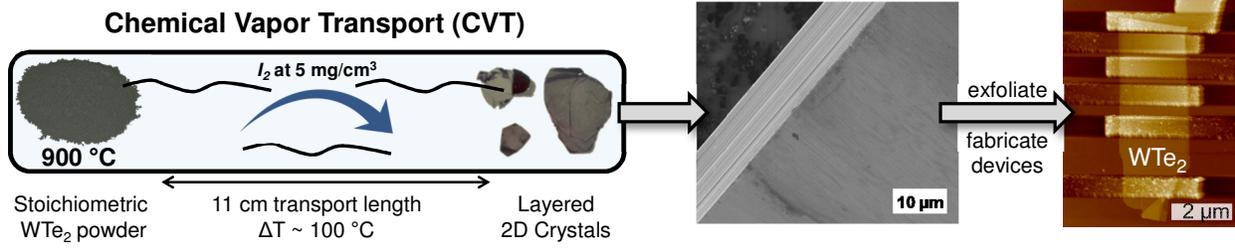


Figure S1. Schematic of CVT growth (see Methods) resulting in mm-size crystals, which are exfoliated into ultra-thin flakes (3-20 layers) to produce the devices studied in this work.

2. Electrical Characterization

Figure S2a demonstrates the independence of Ohmic behavior in few-layer WTe_2 flakes on electrostatic gating, with minute variation in DC current across $V_G = -38$ to $+38\text{ V}$ sweep of a global back-gate (90 nm SiO_2 on $\text{p}^{++}\text{ Si}$). Such invariance was reproduced across all layer thicknesses and temperatures in the 80-300 K range, on both capped and uncapped samples.

Figure S2b demonstrates representative dependence of low-field resistivity vs. temperature (ρ vs. T) for both capped and freshly exfoliated, uncapped flakes in the Ohmic regime. A cubic polynomial fit can be made to both curves (dashed lines), as is implemented in the described self-heating model (Figure 4c). Monotonic increase in resistivity with temperature is consistent with metallic transport.

Figure S2c presents the temperature dependence of contact resistance (R_C), extracted as one-half of the y-intercept in Transfer Length Measurements (TLM) of total resistance vs. channel length (Figure 3a,c). R_C increases monotonically with temperature, but its dependence is less strong than that of resistivity ρ (Figure 3b and S2b). Both ρ and R_C show no clear dependence on layer number. This is consistent with the prior discussions of a relatively 3-dimensional (3D) electron Fermi surface in this structurally 2D material, in addition to the different crystalline orientation of the devices.

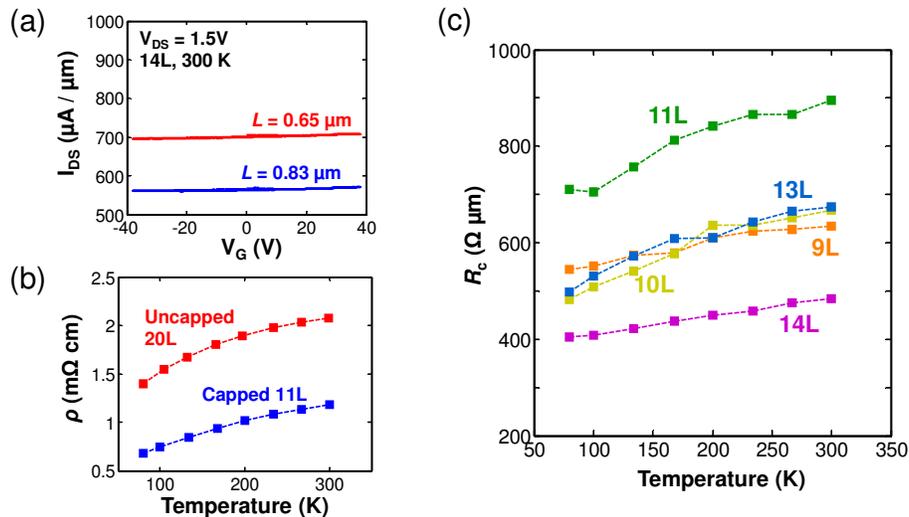


Figure S2. (a) Lack of gate voltage dependence for an AlO_x capped 14 layer WTe_2 flake on 90 nm SiO_2 and $\text{p}^{++}\text{ Si}$ global back-gate, showing negligible current modulation. (b) Comparative temperature-dependent resistivity of newly made capped and uncapped flakes, fit with a cubic polynomial model (dashed lines). (c) Temperature dependence of TLM-extracted R_C for AlO_x -capped WTe_2 multilayers.

3. Thermal Conductivity Estimates

A schematic of the heat flow pathways of WTe₂ devices on 90 nm SiO₂ and Si substrates is provided in Figure 4a of the main text. The average temperature rise of a “long” device ($L \gg L_T$) is $\Delta T = T - T_0 = P\mathcal{R}_{th}$ where P is the input power (i.e. Joule heating), \mathcal{R}_{th} is the overall thermal resistance, and T_0 is the ambient temperature. As described in the main text with further details provided below, the thermal resistance \mathcal{R}_{th} has temperature dependence through the thermal conductivity of SiO₂ (k_{ox}) and the thermal conductivity of the doped silicon substrate (k_{Si}). Their evolution with temperature T can be captured analytically as $k_{ox} = \ln(T_{ox}^{0.52}) - 1.687$ and $k_{Si} = 2.4 \times 10^4 / T_0$, where the average temperature of the SiO₂ is $T_{ox} = (T + T_0)/2$ and the substrate is assumed at the ambient temperature T_0 .¹ This enables a simple iterative solution of the average device temperature T , obtained self-consistently with $k_{ox}(T)$, $k_{Si}(T)$, and the measured device resistivity $\rho(T)$, which is also a function of the average device temperature.

The current is calculated as a function of temperature, $I(T) = V/R(T)$, self-consistently with the self-heating (SH) model whose input are the power $P = I(T)V$ and thermal resistance $\mathcal{R}_{th}(T)$. The input power may be corrected for the voltage lost at the contacts, i.e. $P = I(V - 2IR_C)$.

Following previous work on Joule heating in graphene nanoribbons (GNRs),^{2,3} we can express the peak (max) temperature along the WTe₂ device as a function of input power and other thermal parameters as:

$$T_{max} = T_0 + P \left(\frac{1}{gL} \right) \left(\frac{1 + gL_H R_T x - 1 / \cosh[L/(2L_H)]}{1 + gL_H R_T x} \right) \quad (S1)$$

where $x = \tanh[L/(2L_H)]$. Similarly, we can also express the average temperature (T_{avg}) along the WTe₂:

$$T_{avg} = T_0 + P \left(\frac{1}{gL} \right) \left(\frac{1 + gL_H R_T x - 2x L_H / L}{1 + gL_H R_T x} \right) \quad (S2)$$

In the limit of a “long” device ($L \gg L_H$), the expressions above reduce to $T \approx T_{avg} \approx T_{max} = T_0 + P/(gL)$ and g is described in the main text. If the WTe₂ channel width is small (comparable to the thickness of back-gate SiO₂ thickness 90 nm), the fringing effect of heat loss to the SiO₂ substrate must be considered. We adjust for an effective width $W_{eff} = W + 2t_{ox}$ instead of measured width W to describe this fringing effect (as shown by lateral arrows representing the neat heat diffusion pathway in Figure 4b). In the Equation S1 and S2, R_T is the thermal resistance of the metal contacts, L_H is the thermal healing length along the WTe₂, as described in the main text. Comparing this simple model with temperature-dependent I - V data (Figure 4a), we can estimate the WTe₂-SiO₂ contact thermal resistance, $\mathcal{R}_{Cox} \sim 3 \times 10^{-8} \text{ m}^2 \text{ KW}^{-1}$ in the temperature range 80–150 K. This simple estimate is possible because for “long” devices the heat sinking occurs almost entirely into the substrate and the contacts play very little role.

In the limit of a “short” device (L comparable to or shorter than L_H) heat sinking can occur both into the substrate and into the two contacts. By calculating the lateral heat sinking component we can estimate the lateral thermal conductivity of WTe₂. We note that our devices were capped with AlO_x, which means that lateral heat flow is given by an effective thermal conductivity, k_{eff} , which is the parallel combination of heat flow through the WTe₂ and AlO_x capping layer (see Figure 4a). k_{eff} enters the equations above through the lateral thermal healing length, $L_H = (k_{eff} W t / g)^{1/2}$. The actual value of WTe₂ thermal conductivity is deduced as $k = k_{eff} - k_{cap}(t_{cap}/t)$, where $k_{cap} \approx 4 \text{ Wm}^{-1}\text{K}^{-1}$ (near T_{max}) is the thermal conductivity of AlO_x and $t_{cap} \approx 15 \text{ nm}$ its thickness.^{4,5}

As in previous studies of Joule heating in GNRs,^{2,3} we can estimate the lateral thermal conductivity k of WTe₂ by taking advantage of electrical I - V measurements taken up to device breakdown, reaching $T_{max} \approx$

1300 K (see Section 4 below). We use only “short” WTe₂ devices for this estimate, where lateral heat sinking to the contacts plays a non-negligible role through the thermal conductivity k . (As stated earlier, “long” devices sink most of their heat into the substrate.) Using equation S1 above, we simply relate the (maximum) power input at the point of breakdown from the I - V measurements in Figure 4d to the thermal conductivity, which enters equation S1 through the healing length L_H . We use the shorter three devices measured up to breakdown in Figure 4d to fit \mathcal{R}_{Cox} and k at the same time to match $T_{\text{max}} \approx 1300$ K. We note this represents a “high temperature” (near breakdown) thermal conductivity of WTe₂.

Values fit in this manner, listed in Table S1, match devices breakdown profiles consistently:

Table S1. Lateral thermal conductivity of WTe₂ extracted from device breakdown profiles, per values of WTe₂-SiO₂ thermal contact resistance used as a fitting parameter.

\mathcal{R}_{Cox} (m ² KW ⁻¹)	k (Wm ⁻¹ K ⁻¹)
5×10^{-9}	2.5 to 3.5
7.5×10^{-9}	4 to 6
10^{-8}	9 to 11

The lowest extracted k values exceed those measured by Jana et al. (~ 1 Wm⁻¹K⁻¹) on bulk samples,⁶ necessitating a boundary resistance less than one-tenth the $\mathcal{R}_{\text{Cox}} = 3 \times 10^{-8}$ m²KW⁻¹ estimate at 80-150 K. A decline in \mathcal{R}_{Cox} is expected at elevated temperatures, with higher occupation of relevant phonon modes.

4. Electronic Contribution of Thermal Conductivity

The electronic contribution k_e to the net thermal conductivity k of few-layer WTe₂ flakes is calculated by the Wiedemann-Franz Law as $k_e = \sigma LT$, where σ is electrical conductivity, T is temperature, and $L = 2.44 \times 10^{-8}$ W Ω K⁻² is the Lorenz number. Estimated k_e values for WTe₂ devices of varying thickness are shown in Figure S3, extracted for AlO_x-capped few-layer films. This electronic contribution in ultrathin devices is consistent with prior measurements on bulk, polycrystalline samples through a similar Wiedemann-Franz interpretation of crystal resistivity.⁶ Combining these observations with our estimates above, we surmise that total thermal conductivity of WTe₂ is dominated by phonons, but with a non-negligible (10-30%) electronic contribution.

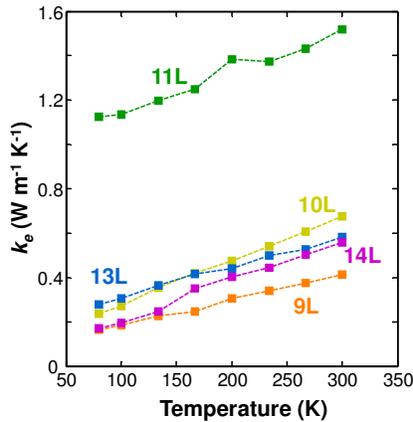


Figure S3. Electronic contribution (k_e) to the lateral thermal conductivity of WTe₂ multilayers vs. temperature. Estimates were made with the Wiedemann-Franz Law from the resistivity directly measured on our TLM structures.

5. Finite Element Simulations

We use finite-element (FE) simulations in COMSOL to verify our analytic thermal model, with results shown in Figures S4 and S5. The FE simulations confirm the predictions of our analytic model, and the ranges of k and \mathcal{R}_{Cox} used therein. Furthermore, the FE simulations also indicate that the device temperature can be reduced by two methods: using a high thermal conductivity material (such as h -BN) as the capping layer, and decreasing the SiO_2 substrate thickness (Figure S4c-d, respectively). h -BN capping provides improved heat spreading to the contacts due to its large in-plane thermal conductivity,⁷ whereas decreasing the SiO_2 thickness reduces the total thermal resistance of the substrate.

Figure S5 directly compares the predictions of the analytic model (dashed lines) and of the COMSOL simulations (symbols). The maximum channel temperature T_{max} vs. applied power P is shown for uncapped, AlO_x capped, and h -BN capped WTe_2 devices on 90 nm SiO_2 , and an AlO_x capped device on 30 nm SiO_2 . Table S2 summarizes how h -BN capping and a thinner SiO_2 substrate could help WTe_2 devices reach higher current densities ($> 50 \text{ MA/cm}^2$) before breakdown.

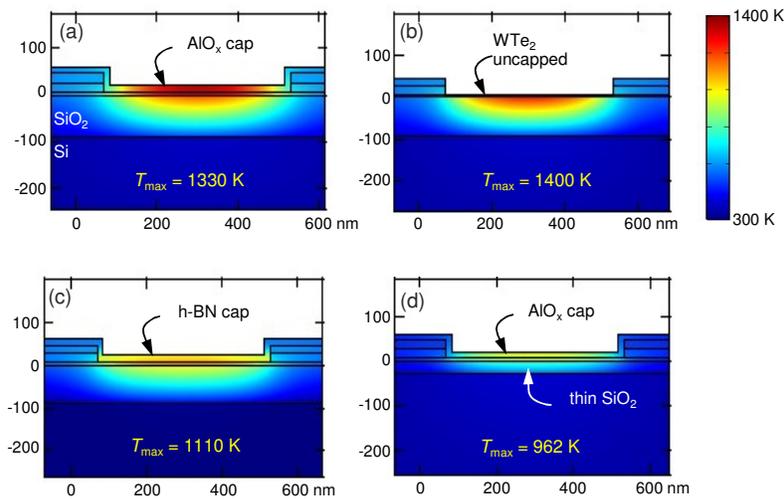


Figure S4. Temperature distribution from finite-element (COMSOL) simulations with 3.55 V applied across a WTe_2 device (dimensions $L = 465 \text{ nm}$, $W = 1.1 \mu\text{m}$ and $t = 6.3 \text{ nm}$). Devices are (a) capped with 15 nm AlO_x as in the experiments, (b) uncapped, and (c) hypothetically capped with 15 nm h -BN (all on 90 nm SiO_2 on an Si substrate). Device (d) is capped with 15 nm AlO_x on 30 nm SiO_2 substrate. The maximum temperature T_{max} in (a) reaches the melting temperature of WTe_2 , consistent with experiments in Figure 4d of the main text and the breakdowns shown in Figure S6. All simulations use temperature-dependent thermal conductivities of Si, SiO_2 and h -BN.

Figure S5. Maximum channel temperature (T_{max}) vs. power input (P) for a WTe_2 device (device dimensions as in Figure S4), comparing analytical model (dashed lines) and simulation results (symbols), validating the use of the analytic model. The same four cases from Figure S4 are studied (uncapped device, capped with AlO_x on 90 nm SiO_2 , capped with h -BN, or capped with AlO_x on 30 nm SiO_2). We use an effective thermal conductivity⁷ for anisotropic h -BN in the analytical model, $k_{\text{BN}} = (k_{\parallel}k_{\perp})^{1/2} \sim 15 \text{ W/m/K}$ (at high temperature, near T_{max}).

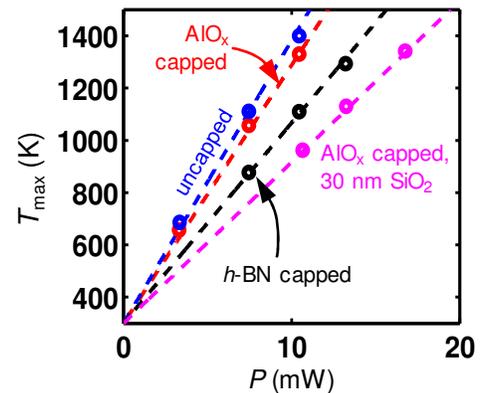


Table S2. Summary of FE simulations, using $k = 10 \text{ Wm}^{-1}\text{K}^{-1}$ and $\mathcal{R}_{\text{CoX}} = 10^{-8} \text{ m}^2\text{KW}^{-1}$ for WTe_2 (device dimensions as in Figure S4), comparing maximum achievable voltages and current densities of $h\text{-BN}$ capped, AlO_x capped and uncapped devices at $T_{\text{max}} \sim 1300 \text{ K}$ (breakdown). The $h\text{-BN}$ capped device achieves the highest current density (J_{max}). Thermal conductivity values are used at high temperature, where data are available, including the anisotropy of k_{\parallel} and k_{\perp} in $h\text{-BN}$.^{5, 7, 8}

Capping material	t_{cap} (nm)	t_{SiO_2} (nm)	k_{cap} (W/m/K)	V_{max} (V)	J_{max} (MA/cm ²)
<i>h</i> -BN	15	90	~ 150 (\parallel , in-plane) ~ 1.5 (\perp , cross-plane)	4	48
AlO_x	15	90	~ 4	3.55	43
AlO_x	15	30	~ 4	4.5	54
none				3.4	41

6. Thermal Breakdown

Figure S6 presents SEM micrographs of few-layer, AlO_x -capped WTe_2 devices following high-current breakdown, imaged at 5 and 10 kV with the SEM mode of a Raith 150. Failure occurs near the mid-point of the channel for all samples, and the Ti/Au electrodes remain fully intact in imaged devices (top and bottom regions of the Figure S6 images). In particular, breakdown around channel centers is consistent with measured metallic conduction, failing nearest the point of highest temperature, T_{max} . In certain short-channel devices, some asymmetry of the breaking point was noted towards a particular electrode, suggesting local field non-uniformity.

Near-complete rupture is observed across the entire width of flakes, alongside apparent local disruption of the encapsulating dielectric layer in certain devices (i.e. both 10L channels). The failure temperature of WTe_2 $T_{\text{max}} \approx 1300 \text{ K}$ is nonetheless 300-400 K below the range for onset of melting in AlO_x , even for amorphous films with small polycrystalline grain size such as those produced by atomic layer deposition (ALD).⁹ Locally defective capping layers may reduce this threshold. Moreover, the WTe_2 melting temperature coincides with the onset of several secondary phenomena, including the boiling point of Tellurium (producing buried gas bubbles which escape by rupturing capping layers),¹⁰ and the formation of Al-Te glasses.¹¹ Volume expansion from the latter reactions may explain the oxide stress visible around failed devices with intact dielectrics (i.e. the 8L device in Figure S6). Our ALD deposition of AlO_x uses H_2O precursor, which leads to Al-rich and sub-stoichiometric oxygen within capping layers.¹² A confluence of these factors likely produces the observed state of post-breakdown devices.

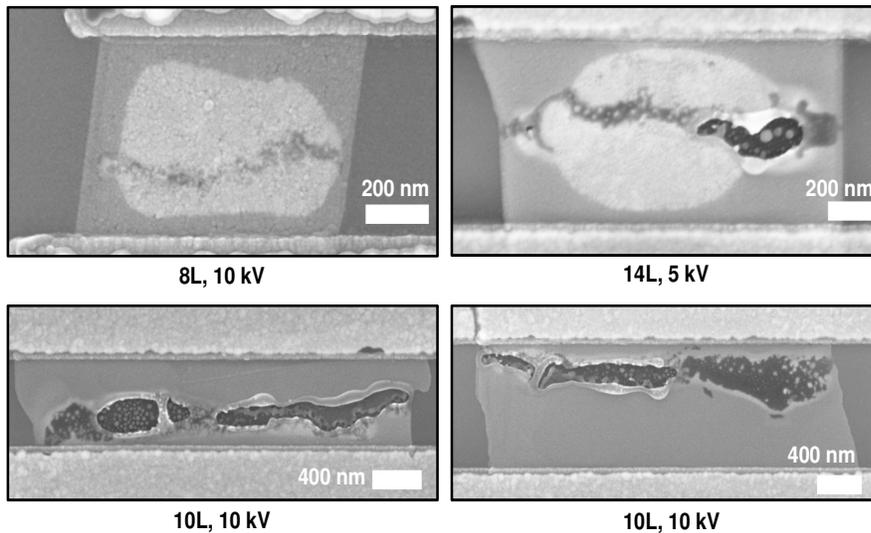


Figure S6. SEM micrographs of AlO_x -capped WTe_2 channels following high-current thermal breakdown, imaged at 5 and 10 kV. Uniform breakdown in channel centers signifies uniform heating during operation and negligible contact resistance. 8 and 10-layer (8L and 10L) samples correspond to devices broken-down in Figure 4d, at respective ambient of $T_0 = 300$ and 80 K.

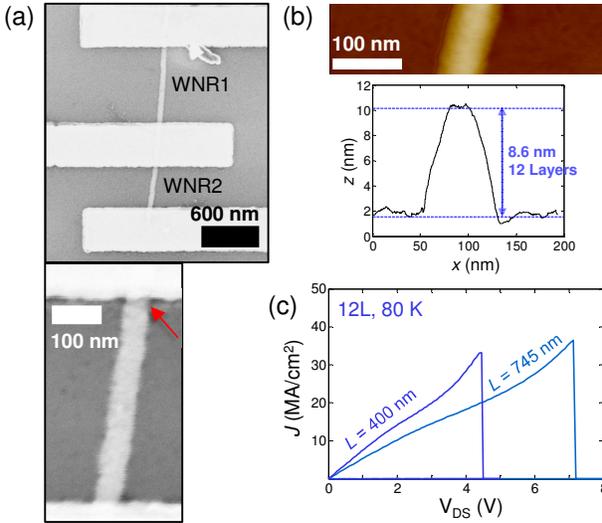


Figure S7. (a) SEM micrographs and (b) AFM micrographs and height profile of a ~ 50 nm wide, 12L thick exfoliated WTe_2 nanoribbon (WNR), capped with AlO_x . Red arrow indicates point of failure. (c) Breakdown current densities of the two WNRs (at 80 K ambient) are comparable to the large WTe_2 device current densities reported in Figure 4d.

Figure S7 shows results of as-exfoliated, 12L WTe_2 nanoribbon (WNR) devices, electrically driven to the point of failure. A mean contact width of ~ 50 nm is estimated by SEM measurements across both channels, with an estimated ~ 5 -10% deviation along the device length. Post-breakdown imaging suggests failure at the Ti/Au contacts (red arrow). Measured current densities (33-37 MA/cm^2 at 80 K ambient) are quite similar to those reported in Figure 4d for wide WTe_2 devices. This is *unlike* short graphene nanoribbons (GNRs) which show *higher* current density than large graphene devices due to their larger thermal healing length which facilitates heat sinking to the contacts (for GNRs).³ This highlights that the current density limitation of short WNRs is intrinsic, due to their low in-plane thermal conductivity.

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